

A generalized Monge-Ampère equation to compute freeform lens surfaces

Karlstad Applied Analysis Seminar, 4 June 2020

Martijn Anthonissen



TU/e

Technische Universiteit
Eindhoven
University of Technology

Computational illumination optics group at TU/e



Jan ten Thije
Boonkkamp



Wilbert
IJzerman
Signify
Research



Martijn
Anthonissen



Maikel
Bertens



Simon
Kronberg



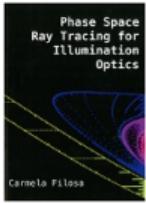
Lotte
Romijn



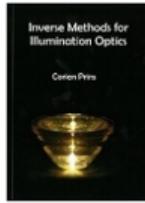
Robert
van Gestel



Teun van
Roosmalen



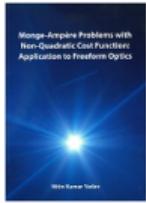
Carmela
Filosa



Corien
Prins



Bart
van Lith



Nitin
Yadav

Outline

Application: Laser beam shaping

Expression for the optical map based on geometrical optics

Energy conservation

Numerical method and results

Concluding remarks

Illumination optics

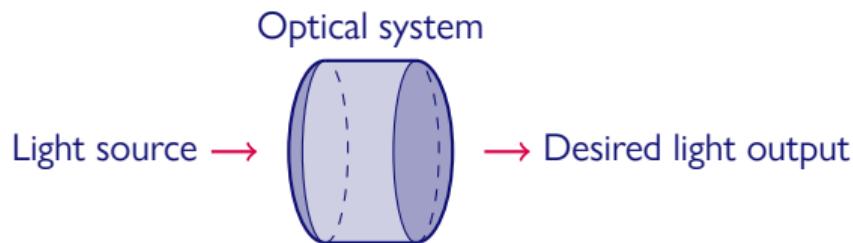
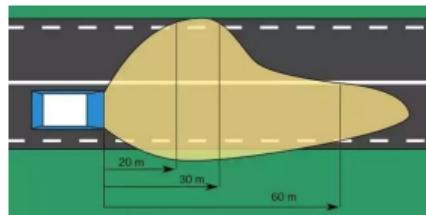
Design of optical systems for illumination purposes

- ▶ LED lighting
- ▶ Road lights
- ▶ Car headlights

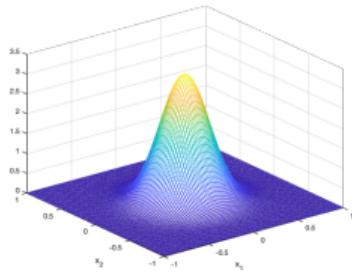
Industry standard: Ray tracing with quasi Monte Carlo methods

- ▶ Easy to implement
- ▶ Slow convergence
- ▶ Design, ray trace, change design, ray trace, ...

Goal: Inverse methods that directly compute the required optical system

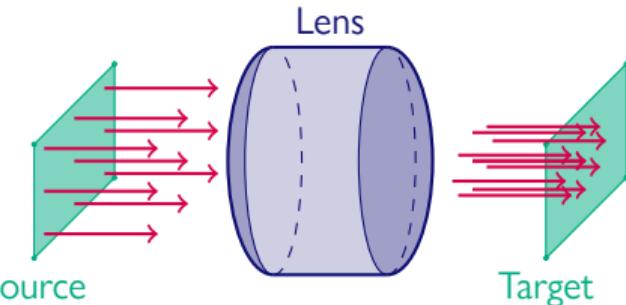


Laser beam shaping

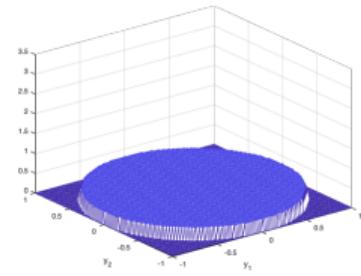


Source distribution:
Gaussian profile

Source emits parallel light rays

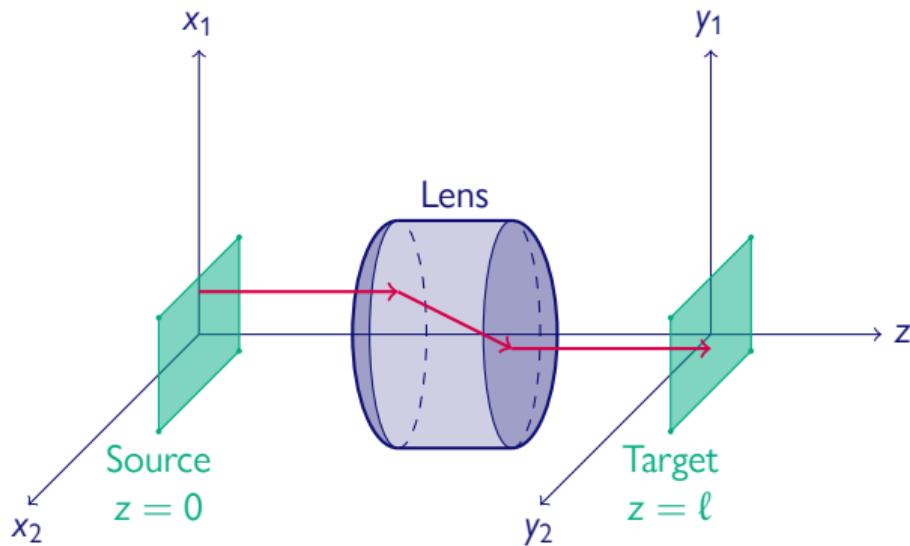


Optical system:
One lens with two freeform surfaces



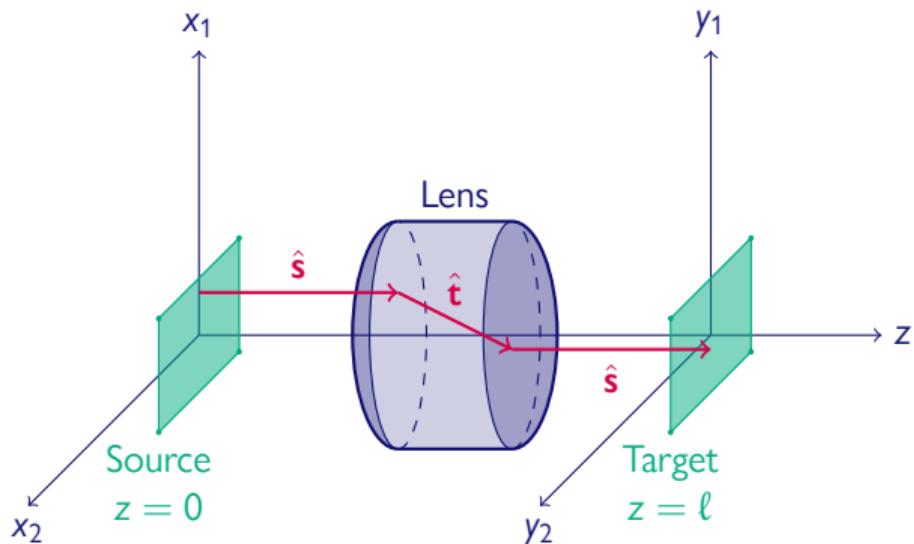
Desired target distribution:
Circular top hat profile
Output beam: Parallel light rays

Laser beam shaping



- ▶ Light rays travel from left to right
- ▶ Source plane: $z = 0$
Cartesian coordinates $\mathbf{x} = \begin{pmatrix} x_1 \\ x_2 \end{pmatrix}$
- ▶ Source S emits parallel light rays
Exitance: $f(\mathbf{x}), \mathbf{x} \in S$
- ▶ First lens surface: $z = u_1(\mathbf{x}), \mathbf{x} \in S$
- ▶ Target plane: $z = \ell$
Cartesian coordinates $\mathbf{y} = \begin{pmatrix} y_1 \\ y_2 \end{pmatrix}$
- ▶ Second lens surface: $\ell - z = u_2(\mathbf{y}), \mathbf{y} \in T$
- ▶ Desired irradiance: $g(\mathbf{y}), \mathbf{y} \in T$

Let's follow a ray through the system

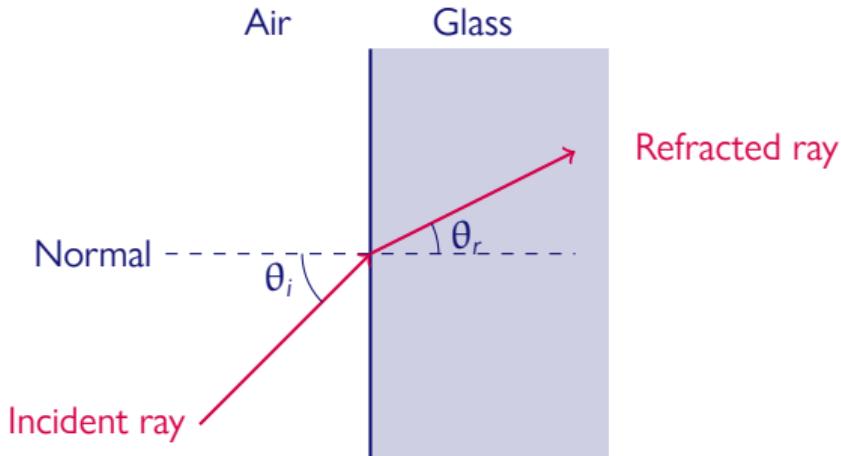


- ▶ Light rays travel from left to right
- ▶ Vectors with length 1 have hat, e.g. \hat{s}
- ▶ Light ray leaves source in direction

$$\hat{s} = \hat{e}_z = \begin{pmatrix} 0 \\ 0 \\ 1 \end{pmatrix}$$

- ▶ Refraction at first lens surface
Refracted (or transmitted) ray has direction \hat{t}
- ▶ Refraction at second lens surface
Ray has direction \hat{s} again

Refraction at lens surface: Snell's law



► Snell's law:

$$n_{\text{air}} \sin \theta_i = n_{\text{glass}} \sin \theta_r$$

► Vector form:

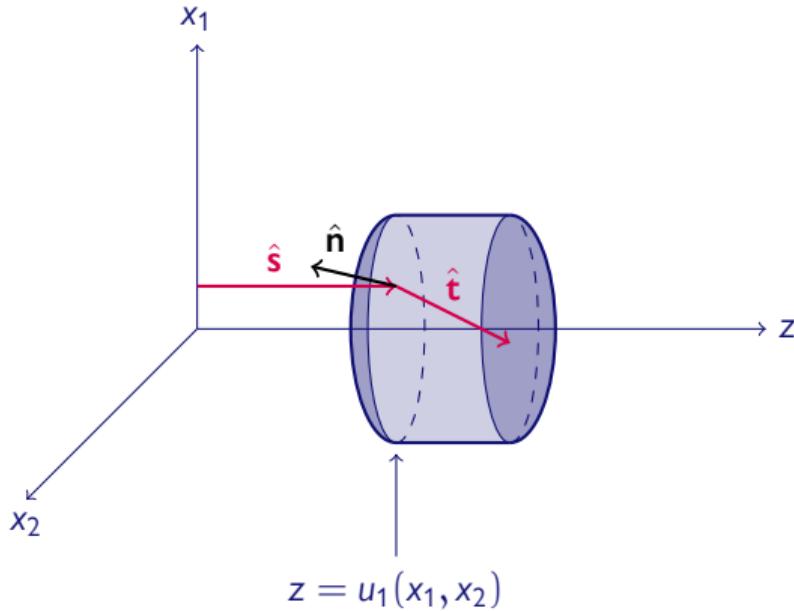
$$\hat{\mathbf{t}} = \alpha \hat{\mathbf{s}} + \beta \hat{\mathbf{n}}$$

with

$$\alpha = \frac{n_{\text{air}}}{n_{\text{glass}}} =: \eta$$

$$\beta = \eta c - \sqrt{1 - \eta^2(1 - c^2)}, \quad c := -\hat{\mathbf{n}} \cdot \hat{\mathbf{s}}$$

Snell's law at the first lens surface



- ▶ Snell's law:

$$\hat{t} = \alpha \hat{s} + \beta \hat{n}$$

$$\alpha = \eta = \frac{n_{\text{air}}}{n_{\text{glass}}}$$

$$\beta = \eta c - \sqrt{1 - \eta^2(1 - c^2)}, \quad c := -\hat{n} \cdot \hat{s}$$

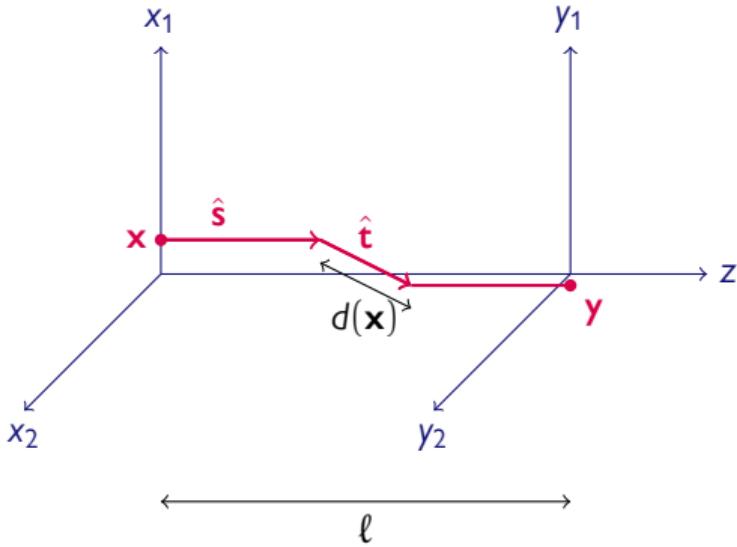
- ▶ First lens surface is $z = u_1(x_1, x_2)$, so

$$\hat{n} = \frac{1}{\sqrt{u_{x_1}^2 + u_{x_2}^2 + 1}} \begin{pmatrix} \frac{\partial u_1}{\partial x_1} \\ \frac{\partial u_1}{\partial x_2} \\ -1 \end{pmatrix}$$

- ▶ Together with $\hat{s} = (0, 0, 1)^T$, we can write

$$\begin{pmatrix} t_1 \\ t_2 \end{pmatrix} = (\eta - t_3) \begin{pmatrix} \frac{\partial u_1}{\partial x_1} \\ \frac{\partial u_1}{\partial x_2} \end{pmatrix} = (\eta - t_3) \nabla u_1$$

Optical map



- We can now write the *optical map* \mathbf{m} as:

$$\mathbf{y} = \mathbf{m}(\mathbf{x}) = \mathbf{x} + \begin{pmatrix} t_1 \\ t_2 \end{pmatrix} d(\mathbf{x})$$

A point $\mathbf{x} \in S$ has image $\mathbf{y} = \mathbf{m}(\mathbf{x}) \in T$

- To find expression for $d(\mathbf{x})$, consider the *optical path length*:

$$L(\mathbf{x}) = n_{\text{air}} u_1(\mathbf{x}) + n_{\text{glass}} d(\mathbf{x}) + n_{\text{air}} u_2(\mathbf{y})$$

Theorem of Malus-Dupin: $L(\mathbf{x}) = L$

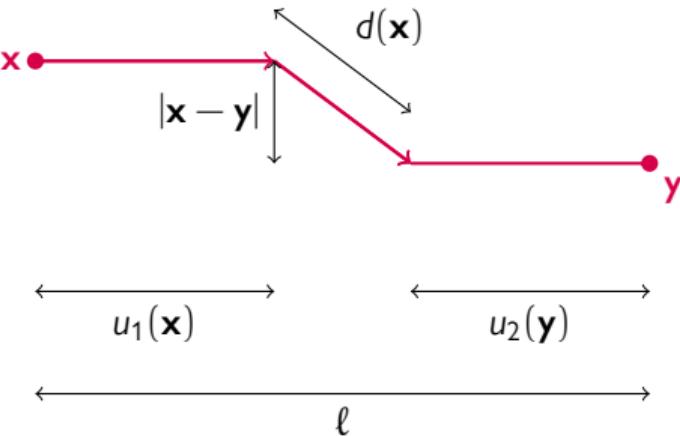
- Also:

$$\ell = u_1(\mathbf{x}) + \hat{\mathbf{s}} \cdot \hat{\mathbf{t}} d(\mathbf{x}) + u_2(\mathbf{y}) = u_1(\mathbf{x}) + t_3 d(\mathbf{x}) + u_2(\mathbf{y})$$

- Conclusion:

$$\mathbf{m}(\mathbf{x}) = \mathbf{x} - \frac{L - n_{\text{air}} \ell}{n_{\text{glass}}} \frac{\nabla u_1(\mathbf{x})}{\sqrt{1 + (1 - \eta^2) |\nabla u_1(\mathbf{x})|^2}}$$

An equation for the freeform lens surfaces



► Pythagoras:

$$|\mathbf{x} - \mathbf{y}|^2 + (\ell - u_1(\mathbf{x}) - u_2(\mathbf{y}))^2 = (d(\mathbf{x}))^2$$

► Optical path length:

$$L = n_{\text{air}}u_1(\mathbf{x}) + n_{\text{glass}}d(\mathbf{x}) + n_{\text{air}}u_2(\mathbf{y})$$

► Rewrite as:

$$u_1(\mathbf{x}) + u_2(\mathbf{y}) = c(\mathbf{x}, \mathbf{y})$$

$$c(\mathbf{x}, \mathbf{y}) = \ell + \frac{n_{\text{air}}}{n_{\text{air}}^2 - n_{\text{glass}}^2} \cdot (L - n_{\text{air}}\ell)$$

$$+ \frac{n_{\text{glass}}}{n_{\text{air}}^2 - n_{\text{glass}}^2} \sqrt{(L - n_{\text{air}}\ell)^2 + (n_{\text{air}}^2 - n_{\text{glass}}^2)|\mathbf{x} - \mathbf{y}|^2}$$

► Optimal mass transport: c is cost function

A special choice for the lens surfaces

- We have found:

$$u_1(\mathbf{x}) + u_2(\mathbf{y}) = c(\mathbf{x}, \mathbf{y})$$

$$c(\mathbf{x}, \mathbf{y}) = \ell + \frac{n_{\text{air}}}{n_{\text{air}}^2 - n_{\text{glass}}^2} \cdot (L - n_{\text{air}}\ell) + \frac{n_{\text{glass}}}{n_{\text{air}}^2 - n_{\text{glass}}^2} \sqrt{(L - n_{\text{air}}\ell)^2 + (n_{\text{air}}^2 - n_{\text{glass}}^2)|\mathbf{x} - \mathbf{y}|^2}$$

- Many possible solutions. We choose a so-called c -convex pair:

$$u_1(\mathbf{x}) = \max_{\mathbf{y} \in T} (c(\mathbf{x}, \mathbf{y}) - u_2(\mathbf{y})), \quad u_2(\mathbf{y}) = \max_{\mathbf{x} \in S} (c(\mathbf{x}, \mathbf{y}) - u_1(\mathbf{x}))$$

- It follows that

$$\nabla_{\mathbf{x}} c(\mathbf{x}, \mathbf{y}) - \nabla u_1(\mathbf{x}) = \mathbf{0}$$

- Substitute $\mathbf{y} = \mathbf{m}(\mathbf{x})$ in previous equation and differentiate once more:

$$D_{\mathbf{x}\mathbf{x}} c(\mathbf{x}, \mathbf{m}(\mathbf{x})) + D_{\mathbf{x}\mathbf{y}} c(\mathbf{x}, \mathbf{m}(\mathbf{x})) D\mathbf{m}(\mathbf{x}) - D^2 u_1(\mathbf{x}) = \mathbf{0}$$

Matrix equation for the Jacobian of the optical map

- ▶ Previous slide

$$D_{xx}c(\mathbf{x}, \mathbf{m}(\mathbf{x})) + D_{xy}c(\mathbf{x}, \mathbf{m}(\mathbf{x})) D\mathbf{m}(\mathbf{x}) - D^2u_1(\mathbf{x}) = \mathbf{0}$$

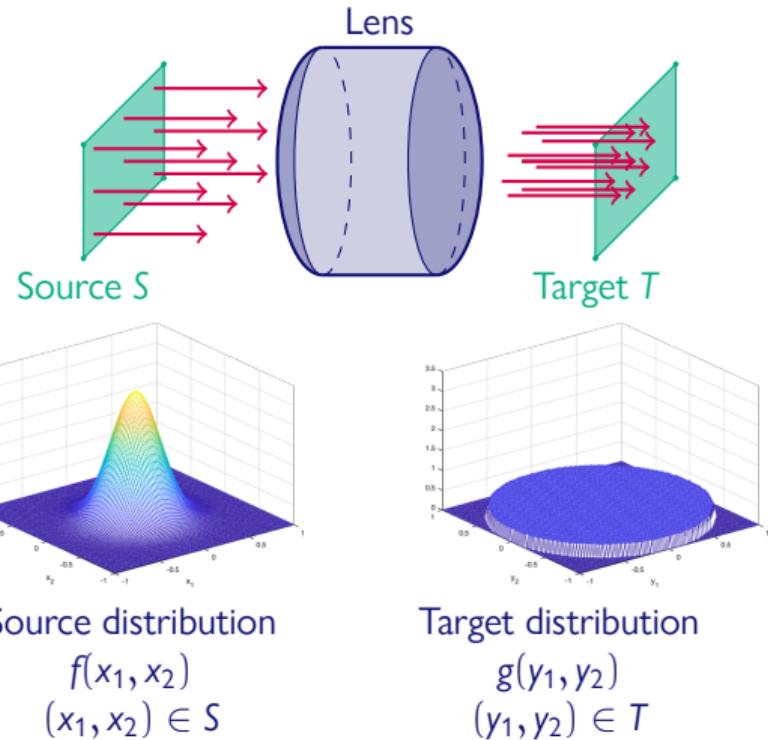
- ▶ Rewrite as

$$\underbrace{D_{xy}c(\mathbf{x}, \mathbf{m}(\mathbf{x}))}_{\mathbf{C}} D\mathbf{m}(\mathbf{x}) = \underbrace{D^2u_1(\mathbf{x}) - D_{xx}c(\mathbf{x}, \mathbf{m}(\mathbf{x}))}_{\mathbf{P}}$$

- ▶ Conclusion:

$$\mathbf{C} D\mathbf{m}(\mathbf{x}) = \mathbf{P}$$

Energy conservation



- ▶ Global energy conservation:

$$\iint_S f(x_1, x_2) dx_1 dx_2 = \iint_T g(y_1, y_2) dy_1 dy_2$$

- ▶ Local energy conservation: For every $A \subseteq S$

$$\begin{aligned} & \iint_A f(x_1, x_2) dx_1 dx_2 \\ &= \iint_{\mathbf{m}(A)} g(y_1, y_2) dy_1 dy_2 \\ &= \iint_A g(\mathbf{m}(x_1, x_2)) \det(D\mathbf{m}(x_1, x_2)) dx_1 dx_2 \end{aligned}$$

- ▶ Differential form:

$$f(\mathbf{x}) = g(\mathbf{m}(\mathbf{x})) \det(D\mathbf{m}(\mathbf{x}))$$

Generalized Monge-Ampère equation

- ▶ Combine matrix equation

$$\mathbf{C} \mathbf{Dm}(\mathbf{x}) = \mathbf{P}$$

with local energy conservation

$$f(\mathbf{x}) = g(\mathbf{m}(\mathbf{x})) \det(\mathbf{Dm}(\mathbf{x}))$$

to find:

$$\det(\mathbf{Dm}(\mathbf{x})) = \frac{\det(\mathbf{P})}{\det(\mathbf{C})} = \frac{f(\mathbf{x})}{g(\mathbf{m}(\mathbf{x}))}$$

Generalized Monge-Ampère equation

- ▶ Transport boundary condition:

$$\mathbf{m}(\partial S) = \partial T$$

- ▶ For simpler optical systems (e.g. single reflector), optical map \mathbf{m} has a potential, so $\mathbf{m} = \nabla \phi$. Then

$$\mathbf{Dm} = D^2\phi = \begin{pmatrix} \frac{\partial^2 \phi}{\partial x_1^2} & \frac{\partial^2 \phi}{\partial x_1 \partial x_2} \\ \frac{\partial^2 \phi}{\partial x_2 \partial x_1} & \frac{\partial^2 \phi}{\partial x_2^2} \end{pmatrix}$$

- ▶ Differential equation:

$$\frac{\partial^2 \phi}{\partial x_1^2} \frac{\partial^2 \phi}{\partial x_2^2} - \left(\frac{\partial^2 \phi}{\partial x_1 \partial x_2} \right)^2 = \frac{f(\mathbf{x})}{g(\mathbf{m}(\mathbf{x}))}$$

Monge-Ampère equation

Numerical method

1. Find the optical map $\mathbf{m} : S \rightarrow T$ from

$$\det(\mathbf{C Dm}) = \frac{f(\mathbf{x})}{g(\mathbf{m}(\mathbf{x}))}$$

$$\mathbf{m}(\partial S) = \partial T$$

2. Find first lens surface $z = u_1(\mathbf{x})$ from

$$\nabla_{\mathbf{x}} c(\mathbf{x}, \mathbf{m}(\mathbf{x})) - \nabla u_1(\mathbf{x}) = \mathbf{0}$$

3. Find second lens surface $\ell - z = u_2(\mathbf{y})$ from

$$u_2(\mathbf{m}(\mathbf{x})) = c(\mathbf{x}, \mathbf{m}(\mathbf{x})) - u_1(\mathbf{x})$$

Numerical method for finding the optical map

- ▶ Find mapping $\mathbf{m} : S \rightarrow T$ such that

$$\det(\mathbf{C} D\mathbf{m}) = \frac{f(\mathbf{x})}{g(\mathbf{m}(\mathbf{x}))}$$
$$\mathbf{m}(\partial S) = \partial T$$

- ▶ Break down in substeps

We compute $\mathbf{P}, \mathbf{b}, \mathbf{m}$ such that

$$\mathbf{P} = \mathbf{C} D\mathbf{m}$$

$$\det(\mathbf{P}) = \frac{f(\mathbf{x})}{g(\mathbf{m}(\mathbf{x}))} \det(\mathbf{C})$$

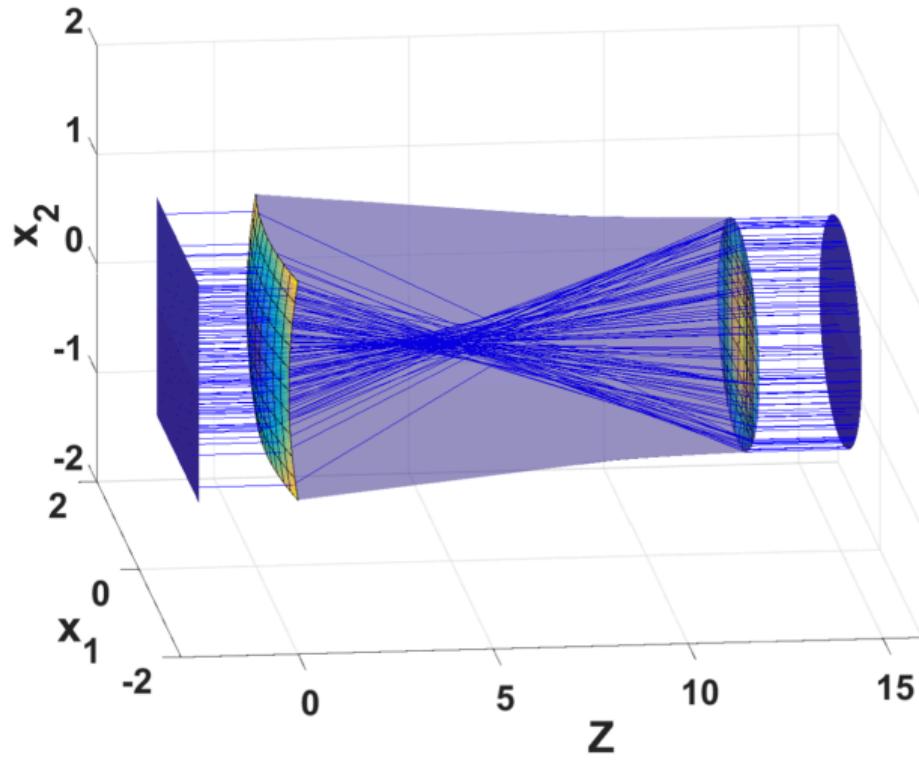
$$\mathbf{b}(\mathbf{x}) = \mathbf{m}(\mathbf{x}), \quad \mathbf{x} \in \partial S$$

\mathbf{b} maps ∂S to ∂T

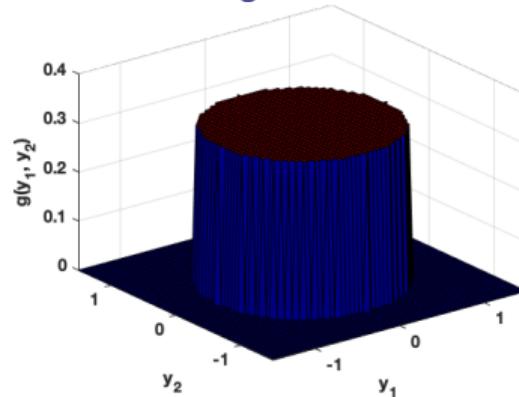
- ▶ Iterative procedure:

1. Choose an initial guess \mathbf{m}^0
Let $n = 0$
2. Let: $J_I(\mathbf{m}, \mathbf{P}) = \frac{1}{2} \iint_S \|\mathbf{CDm} - \mathbf{P}\|^2 d\mathbf{x}$
 \mathbf{P}^{n+1} minimizes $J_I(\mathbf{m}^n, \mathbf{P})$
Constrained minimization problem
3. Let: $J_B(\mathbf{m}, \mathbf{b}) = \frac{1}{2} \int_{\partial S} \|\mathbf{m} - \mathbf{b}\|^2 ds$
 \mathbf{b}^{n+1} minimizes $J_B(\mathbf{m}^n, \mathbf{b})$
Projection on boundary ∂T
4. Let: $J(\mathbf{m}, \mathbf{P}, \mathbf{b}) = \alpha J_I(\mathbf{m}, \mathbf{P}) + (1 - \alpha) J_B(\mathbf{m}, \mathbf{b})$
 \mathbf{m}^{n+1} minimizes $J(\mathbf{m}, \mathbf{P}^{n+1}, \mathbf{b}^{n+1})$
Elliptic PDEs for m_1 and m_2 — FVM

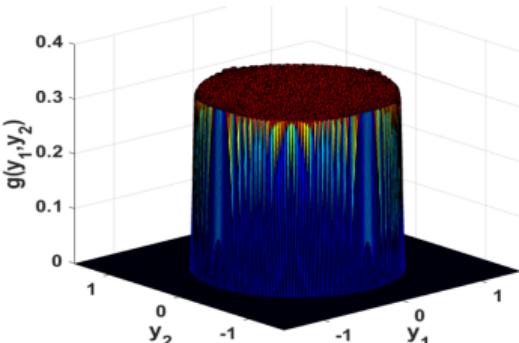
Numerical results for the laser beam shaping problem



Desired target distribution



Achieved



Alternative optical systems

c-convex pair:

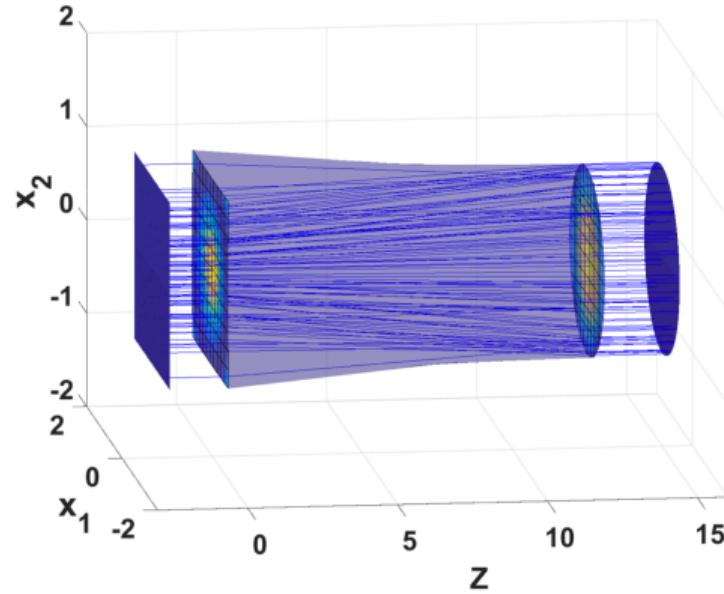
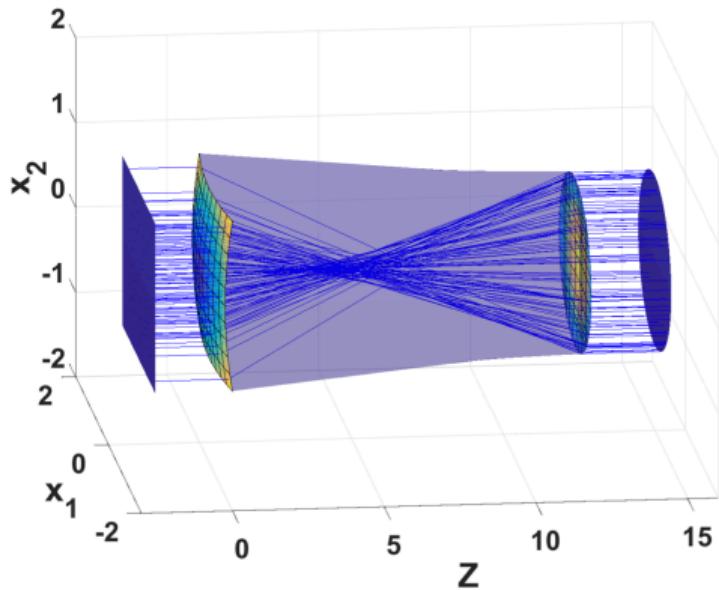
$$u_1(\mathbf{x}) = \max_{\mathbf{y} \in T} (c(\mathbf{x}, \mathbf{y}) - u_2(\mathbf{y}))$$

$$u_2(\mathbf{y}) = \max_{\mathbf{x} \in S} (c(\mathbf{x}, \mathbf{y}) - u_1(\mathbf{x}))$$

c-concave pair

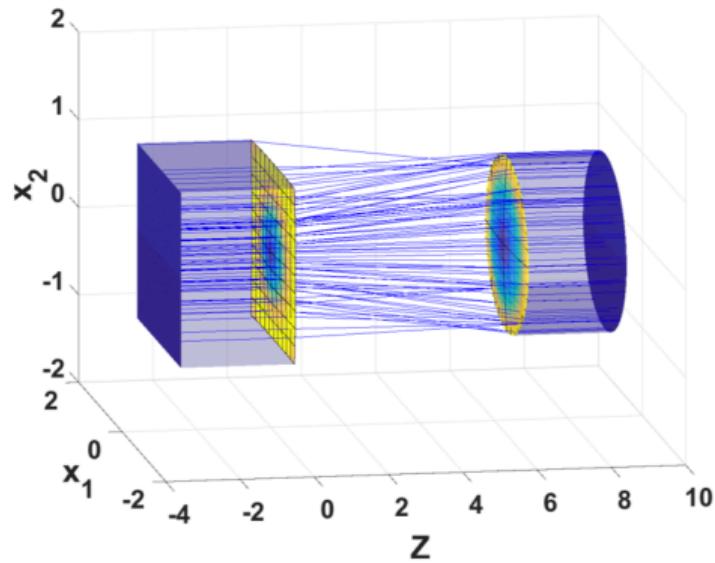
$$u_1(\mathbf{x}) = \min_{\mathbf{y} \in T} (c(\mathbf{x}, \mathbf{y}) - u_2(\mathbf{y}))$$

$$u_2(\mathbf{y}) = \min_{\mathbf{x} \in S} (c(\mathbf{x}, \mathbf{y}) - u_1(\mathbf{x}))$$

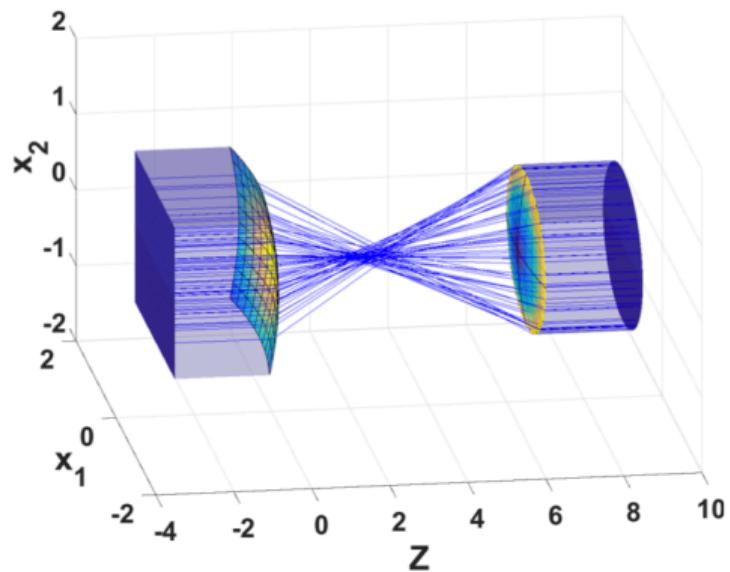


Alternative optical systems (cont)

Two lenses, c-convex

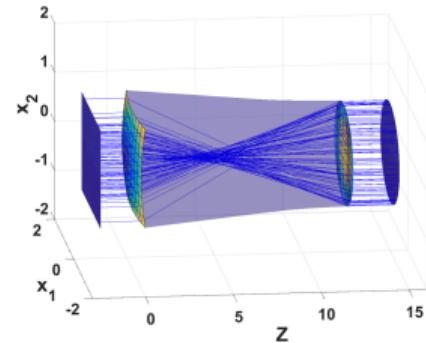


Two lenses, c-concave



Concluding remarks

- Modeled challenging optical design problem
- Based on principles of geometrical optics and energy conservation
- Generalized Monge-Ampère equation with transport boundary condition
- Least-squares solver



More information:

- Yadav, N. K., ten Thije Boonkkamp, J. H. M., IJzerman, W. L. (2019).
Computation of double freeform optical surfaces using a Monge–Ampère solver: Application to beam shaping.
Optics Communications, 439, 251-259. <https://doi.org/10.1016/j.optcom.2019.01.069>
- Yadav, N. K. (2018).
Monge-Ampère problems with non-quadratic cost function: Application to freeform optics.
PhD thesis. Eindhoven University of Technology.